

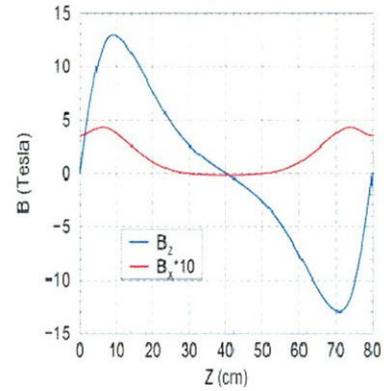
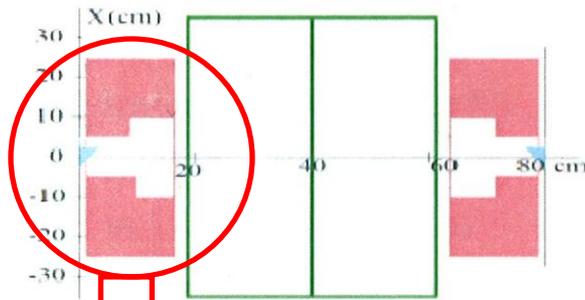
Solenoid for Stage 4 Cooling

I. Novitski, A. Zlobin

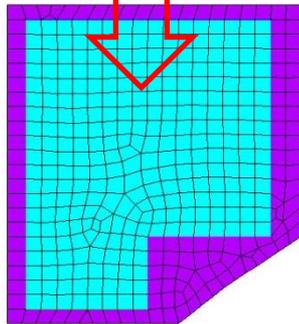
MSD TD

ANSYS Model

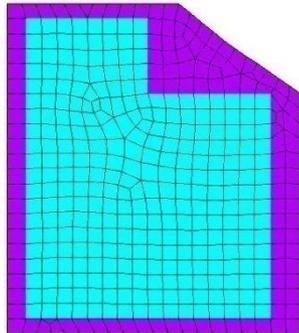
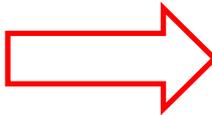
Stage 4



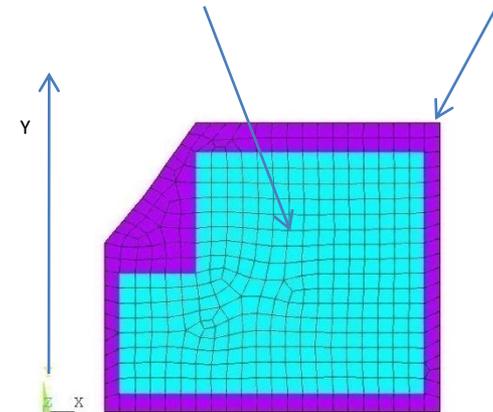
Half-gap: = 1.25 cm



X
x

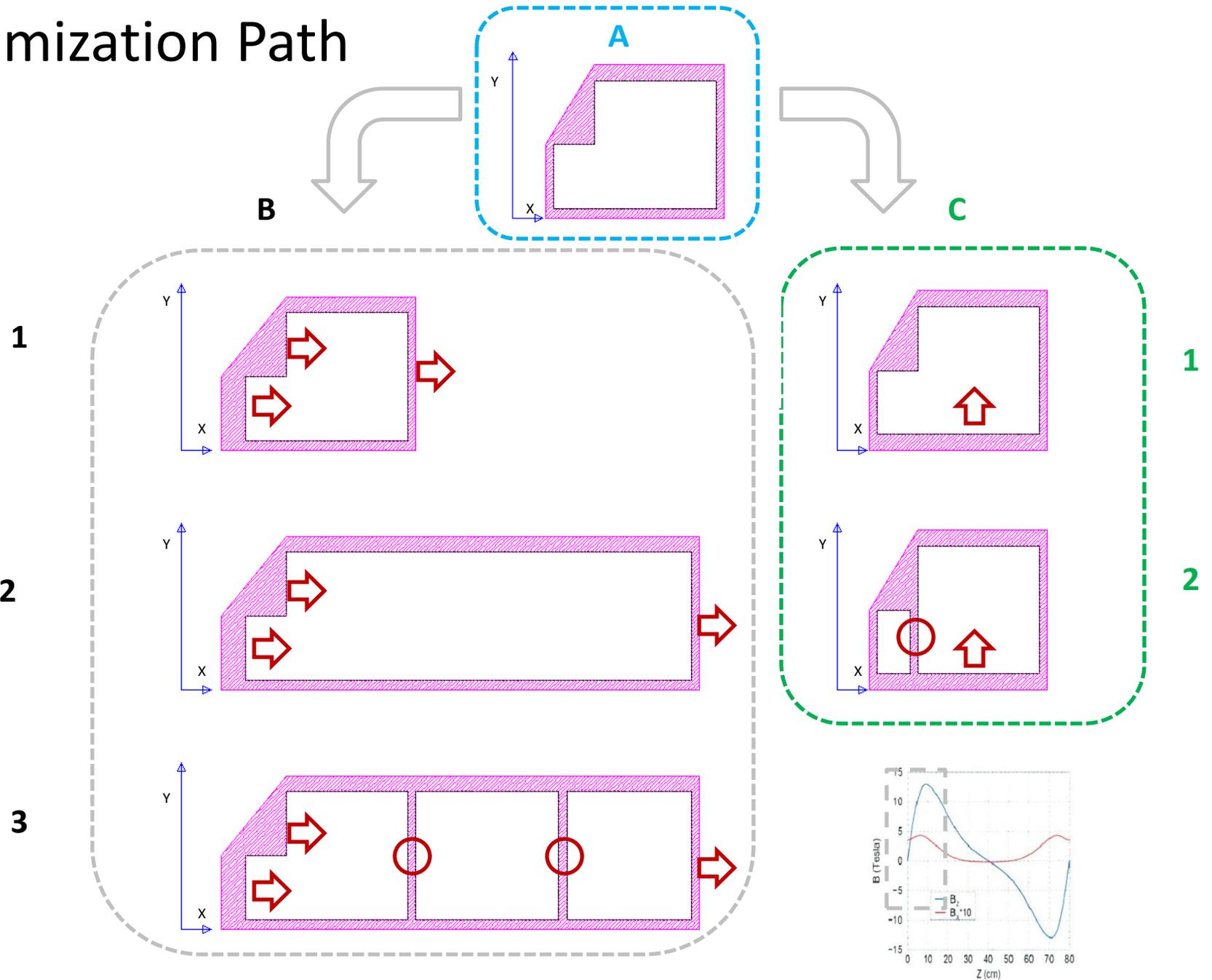


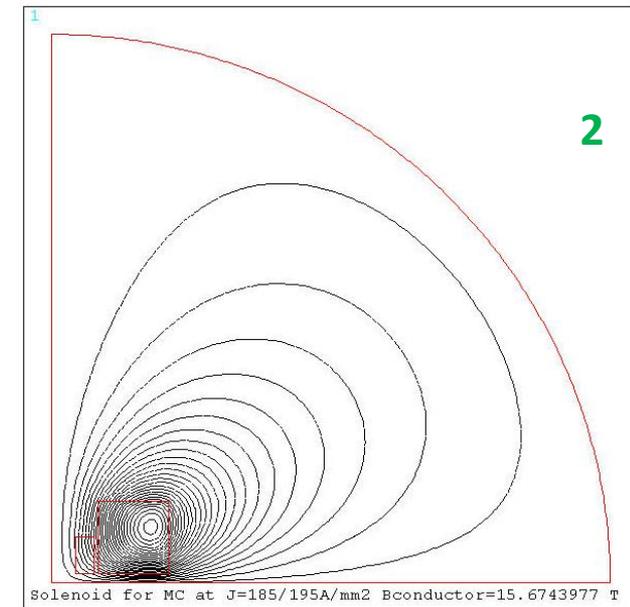
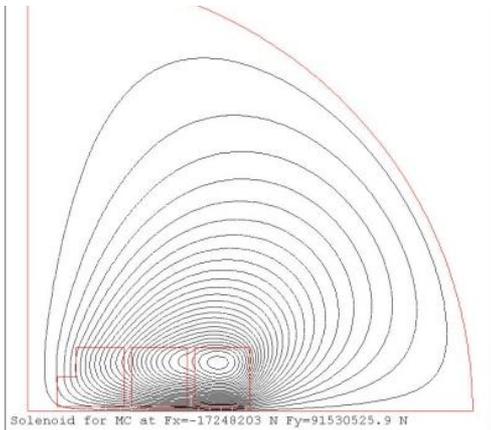
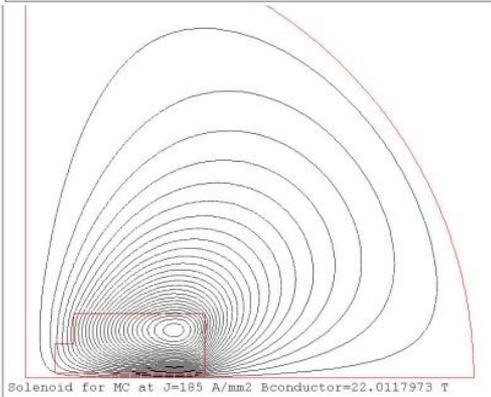
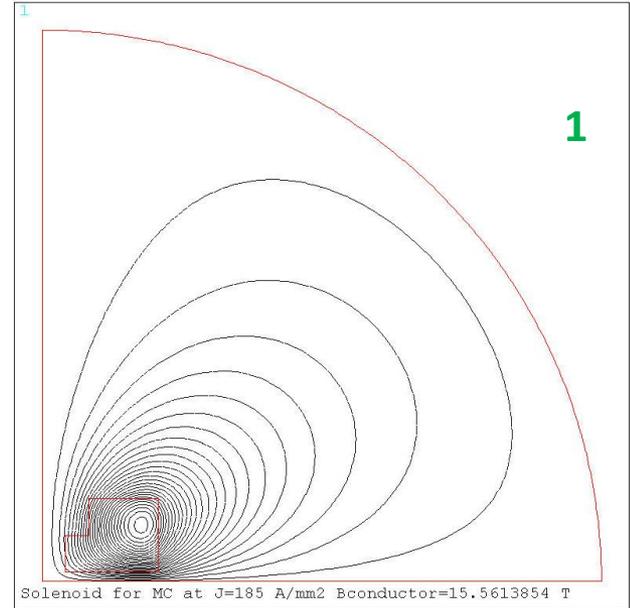
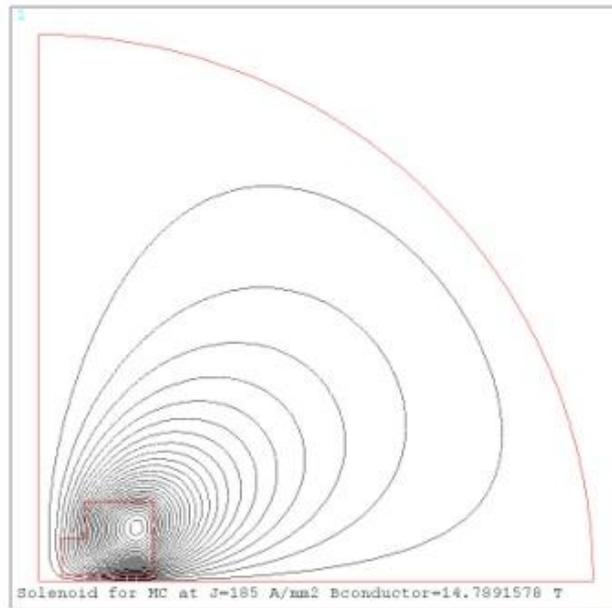
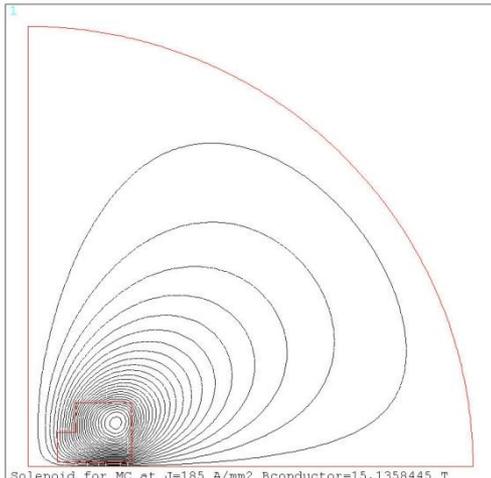
Nb₃Sn Coil SS Frame



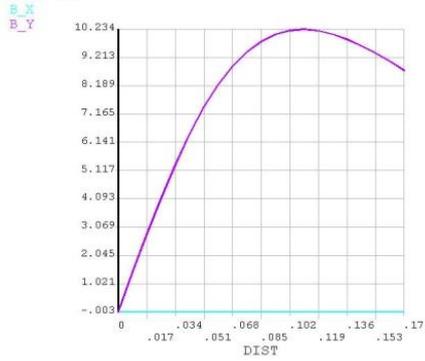
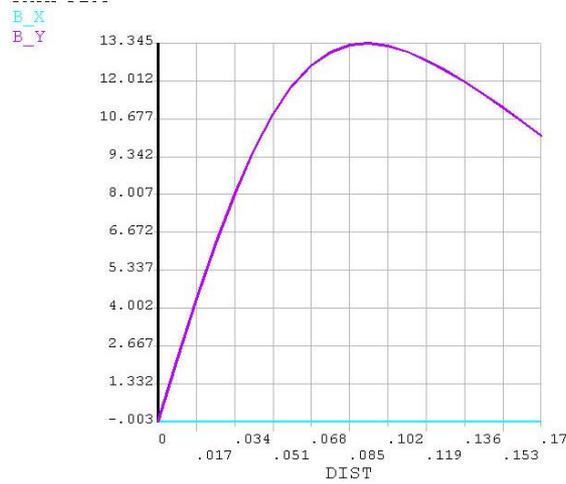
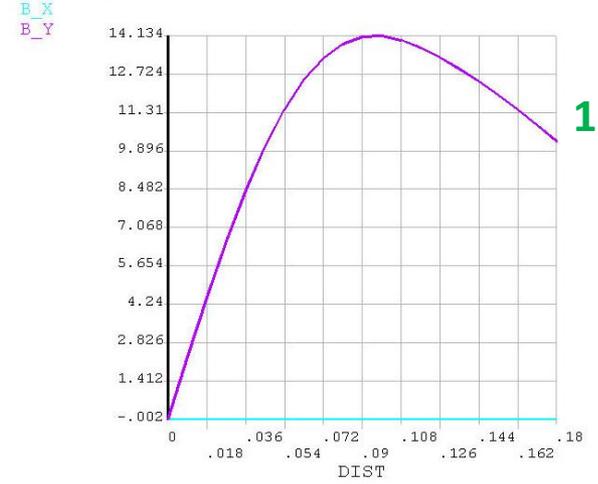
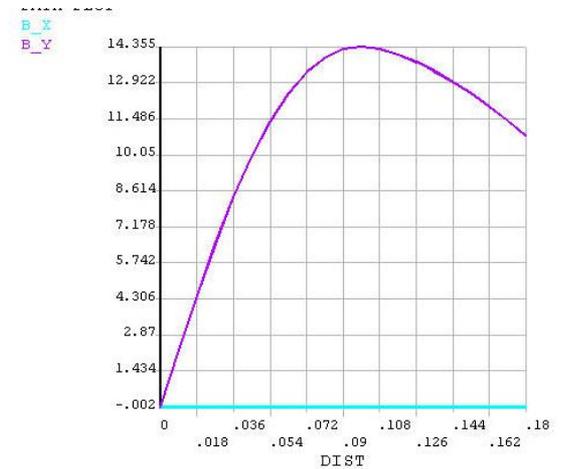
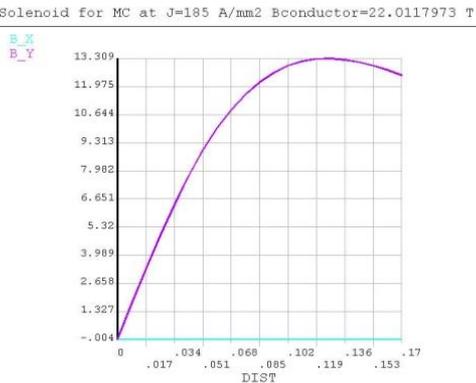
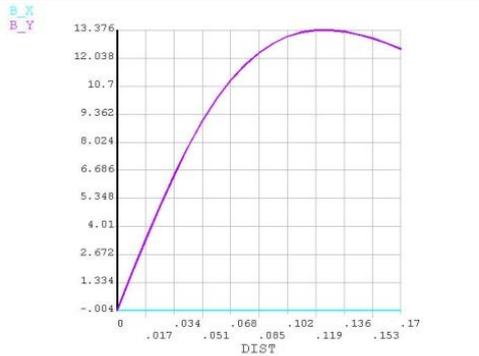
ANSYS Axisymmetrical 2D Model

Optimization Path

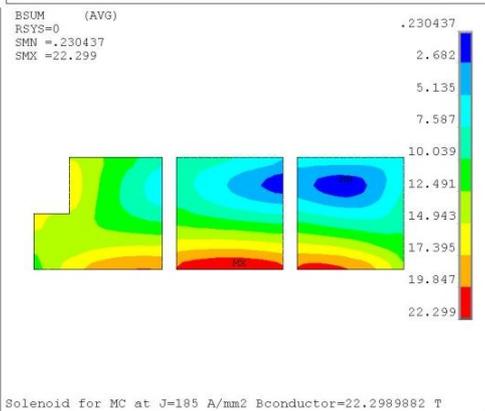
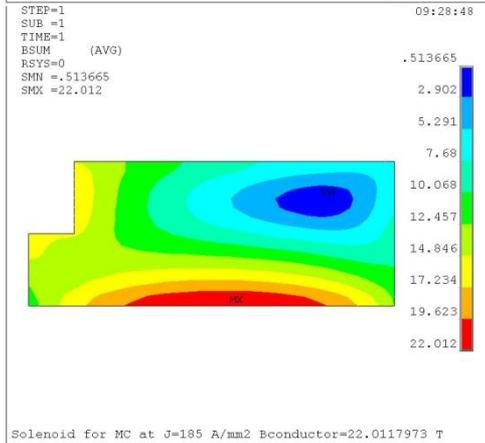
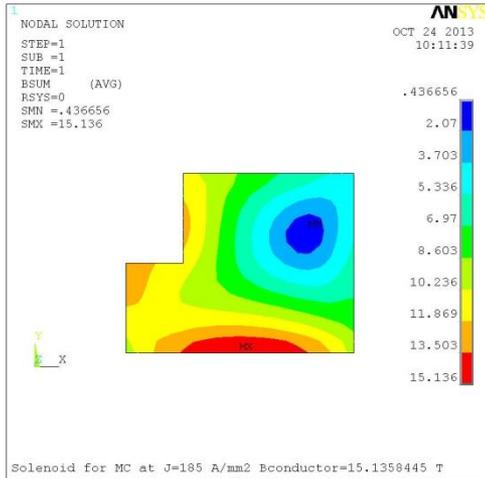
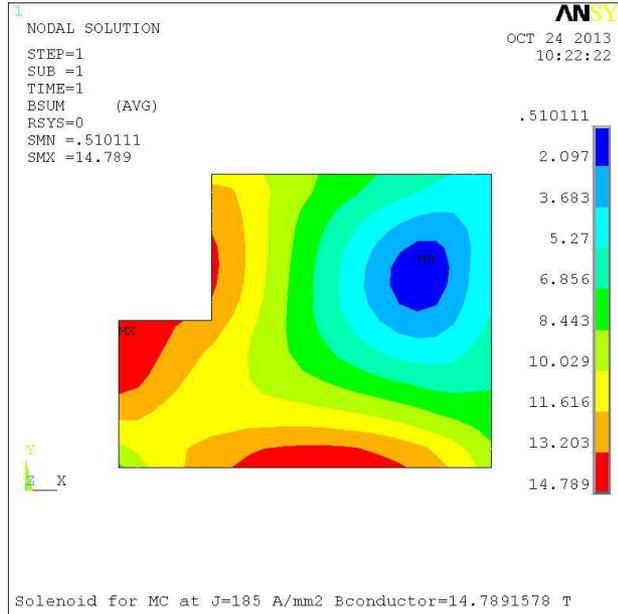
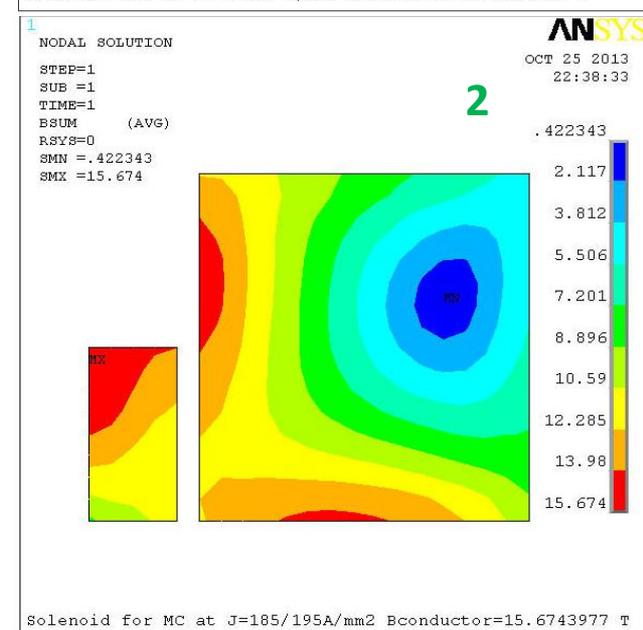
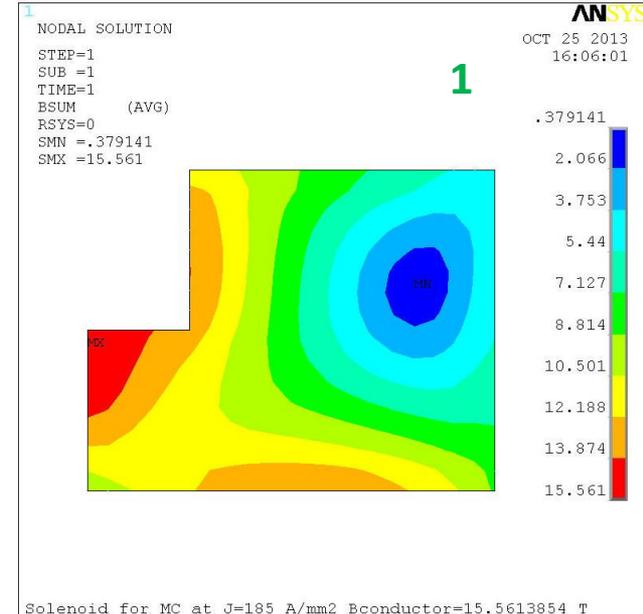


B**A****C**

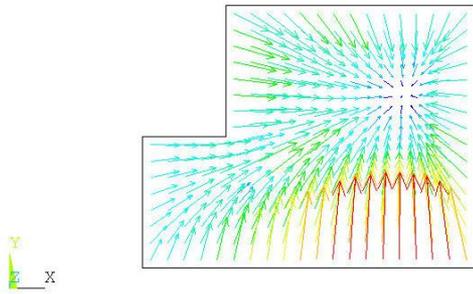
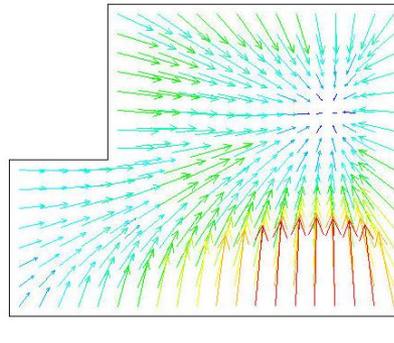
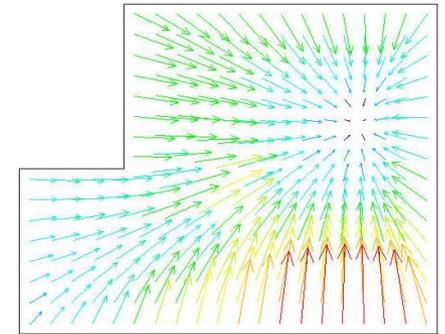
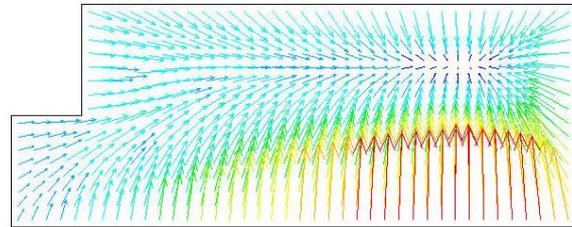
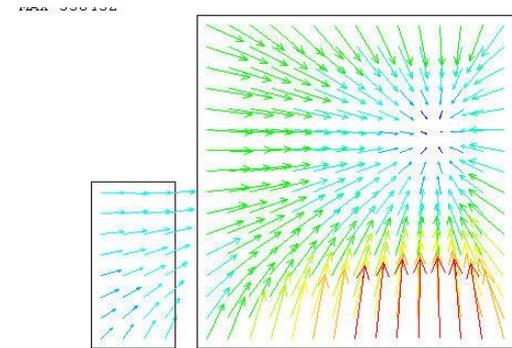
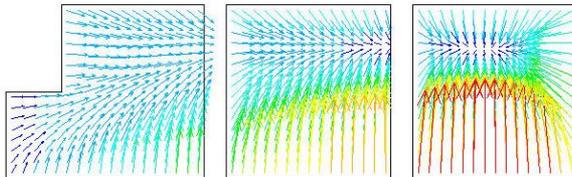
2D Magnetic Flux

B**A****C****1****2**

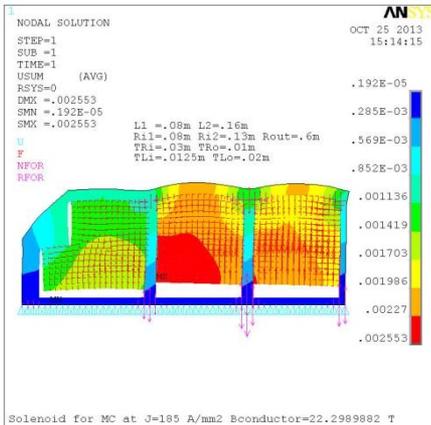
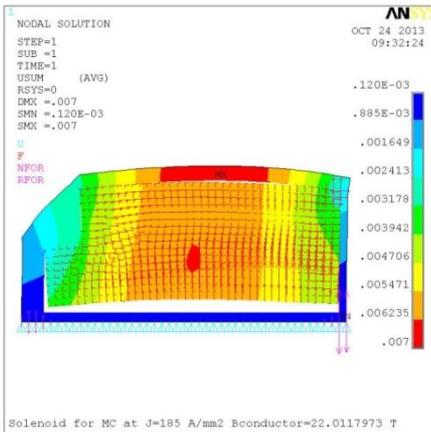
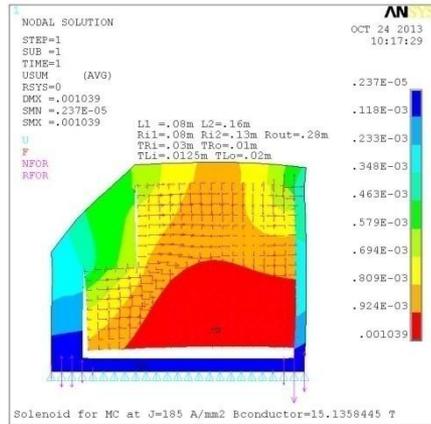
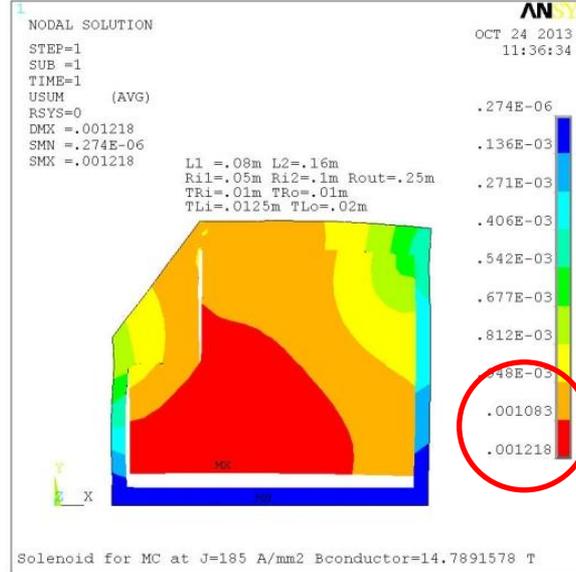
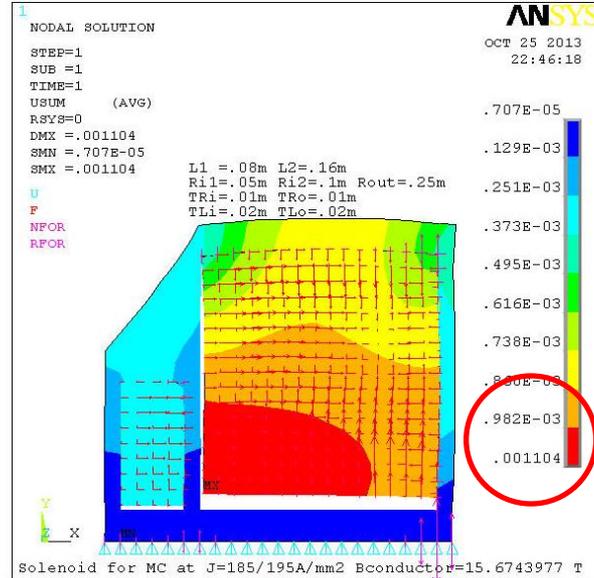
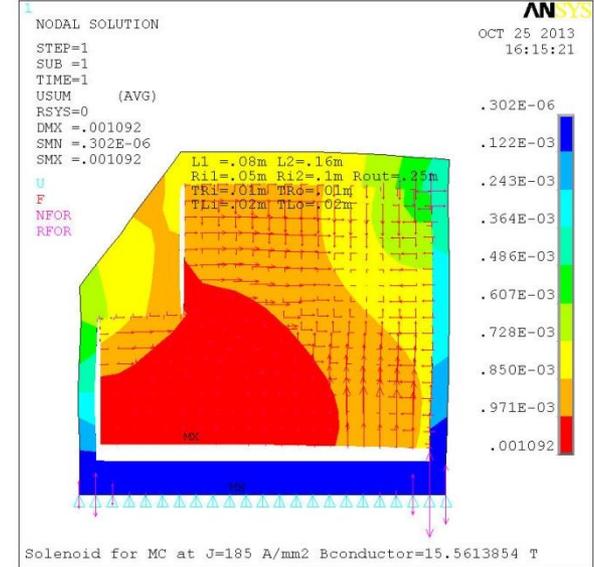
Magnetic Field on Solenoid Axis, T

B**A****C**

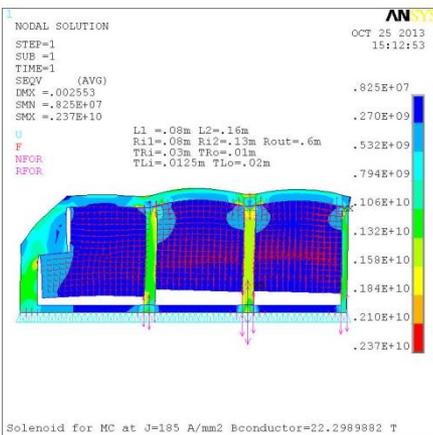
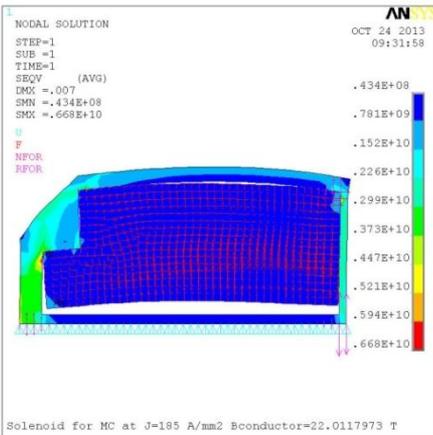
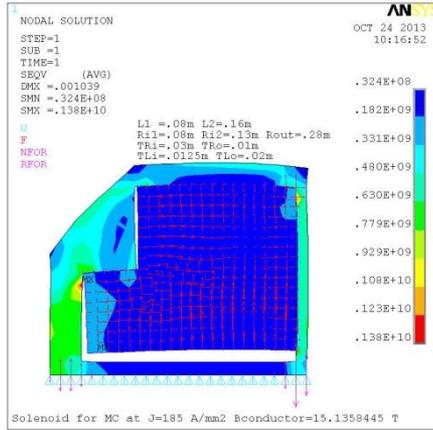
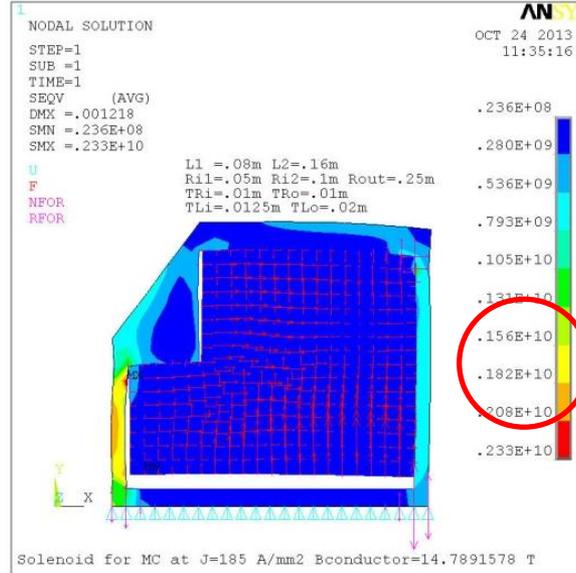
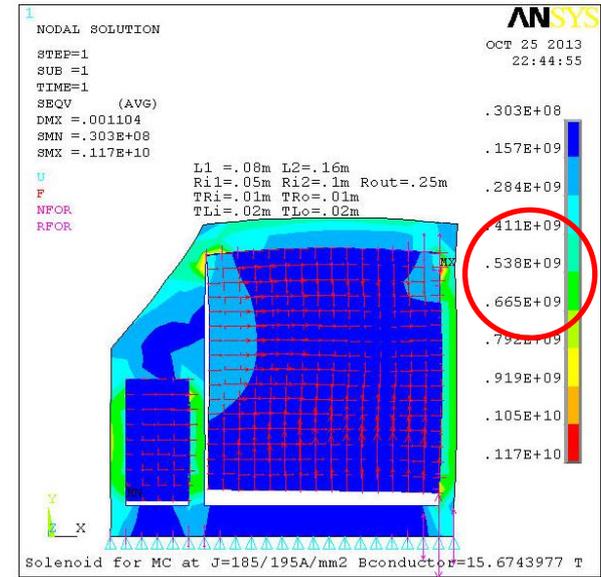
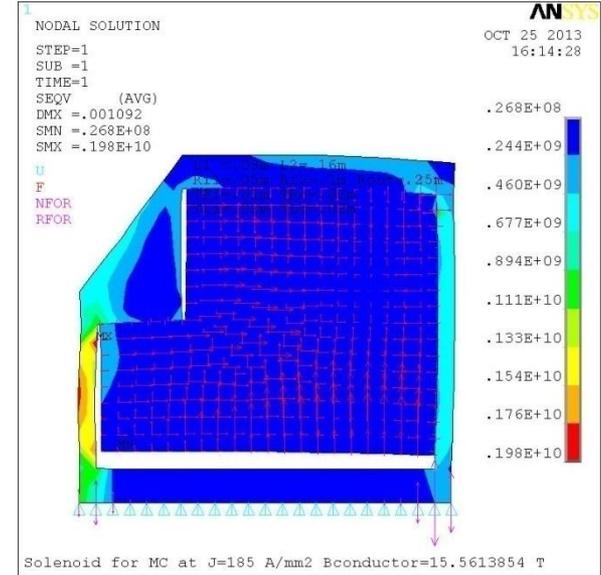
Conductor Magnetic Field, T

B**A****C****1**Solenoid for MC at $F_x=15252428.4$ N $F_y=20994635.5$ NSolenoid for MC at $F_x=14978653.5$ N $F_y=15591758.1$ NSolenoid for MC at $F_x=16222860.9$ N $F_y=13466923.9$ N**1**Solenoid for MC at $F_x=16222860.9$ N $F_y=13466923.9$ N**2**Solenoid for MC at $F_x=49538492.6$ N $F_y=125257033$ N**2****3**Solenoid for MC at $F_x=2878197.43$ N $F_y=1132242.32$ NSolenoid for MC at $F_x=-17248203$ N $F_y=91530525.9$ N

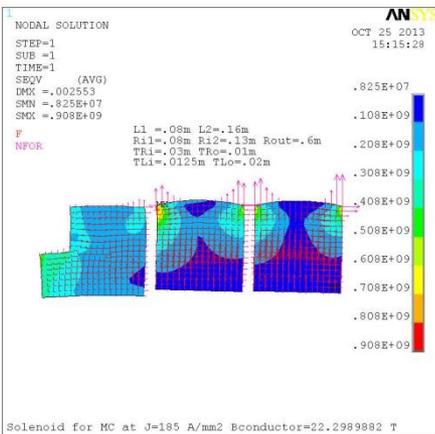
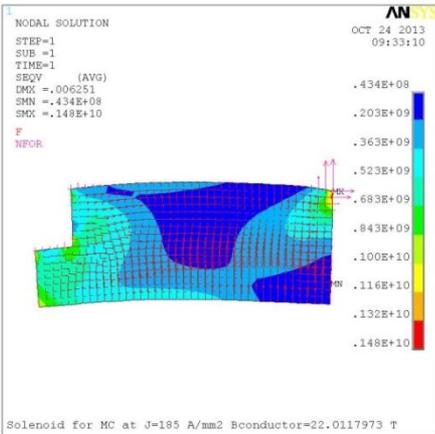
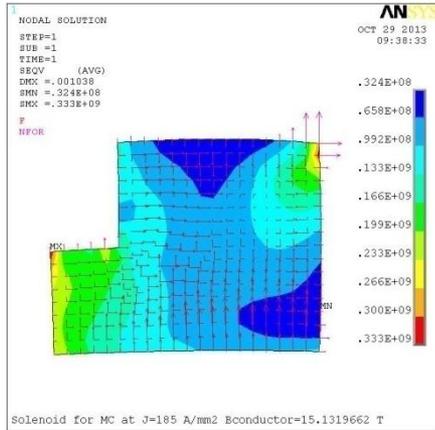
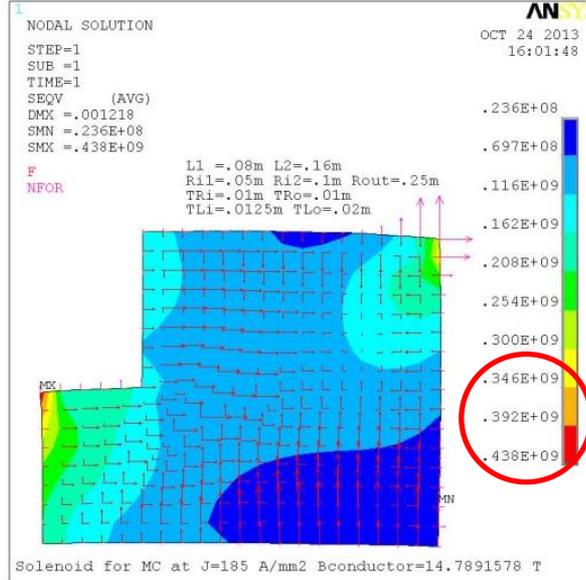
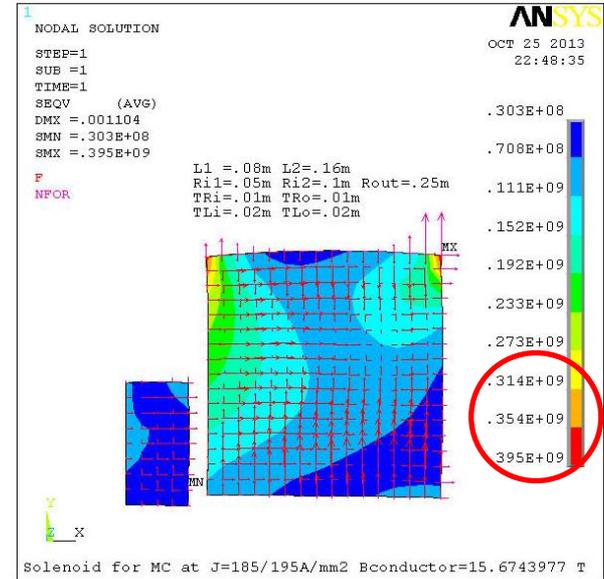
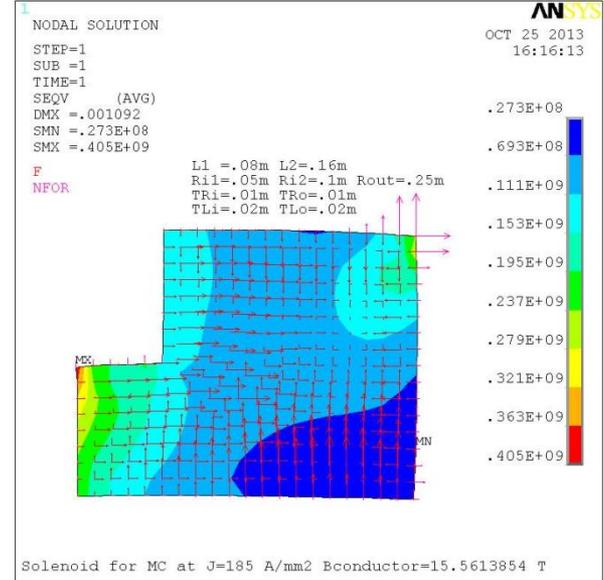
Lorentz Forces, Nm

B**A****C**

Displacement Vector Sum, m

B**A****C**

Equivalent Stress, Pa

B**A****C**

Coil Equivalent Stress, Pa

Summary

Path “B”:

- The “Original Design (A)” required a thicker inner tube wall to reduce carcass stress and coil motion under LF action.
- Increasing wall thickness decreases solenoid bore.
- To preserve the bore diameter, the entire solenoid should be shifted radially outwards.
- Magnetic field on solenoid axis decreases with increasing solenoid inner radius.
- In order to keep the same magnetic field, an increase of coil volume is required.
- Bigger coil volume leads to a bigger outside coil radius, weaker structure, and ribs introduction.
- Ribs divided the coil volume and created an almost identical innermost coil block as in the “Original Design”.
- The new derived design is more complicated than and not as efficient as the original one.

Summary

Path “C”:

- Magnetic field on solenoid axis increases when two solenoids moved apart axially.
- Dividing the coil into two blocks with 10mm coil rib may solve the stress problem in the 10mm inner carcass wall and will keep the original bore diameter.
- Coil displacement is still too large (~1mm); smaller number (0.1mm) is preferred
- Coil stresses should be reduced as well to 150-170MPa level

Next Step

- 3D FEA models are needed for the result verification.
- Using “Conductor in Conduit” may help solving stress-displacement problems since coil rigidity will be increased.